

TITLE OF THE INVENTION

IMPEDANCE TRIMMING CIRCUIT

CROSS-REFERENCE TO RELATED APPLICATIONS

This is a Continuation-in-Part application of
5 US. Patent Application No. 10/608,364, filed
June 26, 2003, the entire contents of which are
incorporated herein by reference.

This application is based upon and claims the
benefit of priority from the prior Japanese Patent
10 Applications No. 2003-113191, filed April 17, 2003;
and No. 2003-307766, filed August 29, 2003, the
entire contents of both of which are incorporated
herein by reference.

BACKGROUND OF THE INVENTION

15 1. Field of the Invention

The present invention relates to an LSI
containing an impedance trimming circuit to execute
impedance matching on output impedance, input
impedance, terminal resistance, or the like to
20 suppress reflection of signals, thus allowing high-
speed serial signals of high quality to be
transferred, and in particular, to a trimming
circuit for accurate and automatic adjustment.

2. Description of the Related Art

25 For a high-speed interface such as a USB2.0 (480
Mbps) or an LUDS (several Gbps), it has hitherto
been essential to match input impedance, drive

impedance, pull-up/pull-down resistance, or the like with a corresponding standard value (for example, $\pm 10\%$) in order to suppress reflection of the waveform of a transferred signal, thus allowing a high-speed signal of high quality to be transmitted.

5 However, resistance elements manufactured using an LSI manufacturing process vary markedly (for example, $\pm 20\%$). Further, the on resistance of an output transistor depends significantly on a temperature, 10 a power voltage, or a threshold (for example, worst best = double/half). Accordingly, a certain adjustment circuit is required.

A first example of the prior art is Non-patent Document 1 (ESSCIRC2001 "A New Impedance Control 15 Circuit for USB2.0 Transceiver" Koo K.-H. SAMSUNG Electronics
http://www.esscirc.org/esscirc2001/C01_Presentations/5.pdf).

In Non-patent Document 1, as shown in FIGS. 1 20 and 2, an operational amplifier adjusts a voltage drop at an external resistor R_{ext} to an internal reference voltage V_{ref} . An output signal from the operational amplifier is supplied to gates of two P channel MOS transistors. An output signal from an output buffer 25 appears as a positive and negative differential outputs at a Data + terminal and a Data - terminal, respectively, on the basis of voltage drops at internal

resistors. This circuit has an auxiliary circuit for adjustment in addition to a circuit for data transfer. The auxiliary circuit finds, in a controlled manner, a code that adjusts the potential at a VA terminal to 5 a value V_{ref} .

In this case, output impedance is based on the internal resistor and MOS resistor. However, in this conventional example, this value is adjusted to $45\Omega \pm 5\Omega$. Specifically, a comparator and a control 10 circuit are used to adjust the sizes of the MOS transistors to find a code that results in the smallest error. Then, the sizes of the MOS transistors are increased or reduced, and this code is provided to the output buffer.

15 However, with this method, the circuit is affected by various variation factors such as a variation in reference voltage, an input offset voltage at the operational amplifier, a variation in the current ratio of a current source composed of the P channel MOS 20 transistors, and a variation in MOS resistance. Thus, actually, it is difficult to accurately adjust the output impedance.

For example, if the current ratio of the current source composed of the P channel MOS transistors varies 25 by about 5%, this mere variation causes the output impedance to reach the limit of the allowable variation range of $45\Omega \pm 5\Omega$. Thus, disadvantageously, yield

decreases and much labor is required to manage manufacturing steps. Therefore, in reality, it is difficult to accurately adjust the output impedance.

A second example of the prior art is Non-patent Document 2 (ESSCIR2001 "Digitally tuneable on-chip line termination resistor for 2.5 Gbit/s LVDS receiver in 0.25 μ m standard CMOS technology" M. Kumric, F. Ebert, R. Rap, K. Welch Alcatel SEL Stuttgart (http://www.esscirc.org/esscirc2001/C01_Presentations/98.pdf)).

10 In Non-patent Document 2, as shown in FIG. 3, a value for an internal trimming resistor is switched so that the externally provided reference voltage V_{ref} is closest to a divided voltage resulting from an external resistor and the internal trimming resistor. 15 Then, switching codes are used to switch input terminal resistance.

As shown in FIG. 4, the internal trimming resistor is composed of a resistor R_0 connected directly between IP and IN and resistors R_1 to R_8 each connected via 20 a switch turned on and off in a controlled manner using a code.

As shown in FIG. 5, in consideration of the range of a variation in the value for the internal resistor, a value for the resistor R_0 is preset at a larger 25 value. The resistors R_1 to R_8 are sequentially connected together to adjust the value for the internal trimming resistor over a wide range so that it falls

within the range of a standard value of $100\Omega \pm 10\Omega$.

However, this method requires an external circuit used to generate the reference voltage V_{ref} as well as two external accurate resistors. This advantageously increases costs. Further, this method is used only for an input terminal section. The adjustment of the output impedance must include the adjustment of the on resistance of the output buffer as shown in the first example of the prior art.

A third example of the prior art is Patent Document 1.

In Patent Document 1 (Jpn. Pat. Appln. KOKAI Publication No. 2001-94048), as shown in FIG. 6, the operational amplifier is used to adjust a current from the current source composed of the P channel MOS transistors so that a voltage drop V_{ZQ} at an external resistor PQ is half the voltage at a power source V_{DDQ} . Further, the size of an output driver is adjusted by using a current mirror to allow a current to flow through the output driver so that the resulting voltage drop equals the V_{ZQ} .

In this case, a variation in output resistance is affected directly by factors such as the offset voltage at the operational amplifier and a variation in current mirror current. Consequently, accurate adjustment of the current is limited.

It has thus been strongly desirable to provide

an impedance trimming circuit which eliminates the adverse effects of variations associated with an LSI manufacturing process to accomplish accurate trimming and which can be constructed using a reduced number of 5 external parts.

BRIEF SUMMARY OF THE INVENTION

According to an aspect of the present invention, there is provided an impedance trimming circuit comprising a common bias section composed of a first 10 series circuit having a first internal resistor and an external resistor connected in series via a first node and a first operational amplifier having a first input terminal connected to an internal reference voltage, a second input terminal connected to the first 15 node, and an output terminal connected to the first series circuit; and an impedance trimming section composed of a second series circuit having a second internal resistor and an impedance dummy resistor connected in series via a second node, a comparator having a first input terminal connected to the first node and a second input terminal connected to 20 the second node, a code control circuit which uses a clock signal to latch an output signal from the comparator to generate a plurality of switching codes, and a switching circuit which uses the plurality of 25 switching codes to switch a resistance value of the impedance dummy resistor, wherein the first operational

amplifier is also connected to the second series circuit, and an output signal from the code control circuit is input to a target impedance trimming resistor.

5 BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

FIG. 1 is a diagram showing a conventional impedance trimming circuit;

FIG. 2 is a diagram showing a conventional impedance trimming circuit;

10 FIG. 3 is a diagram showing a conventional impedance trimming circuit;

FIG. 4 is a diagram showing an example of a conventional trimming resistor;

15 FIG. 5 is a diagram showing the relationship between codes and the resistance value of the trimming resistance;

FIG. 6 is a diagram showing a conventional impedance trimming circuit;

20 FIG. 7 is a diagram showing an impedance trimming circuit according to a first embodiment;

FIG. 8 is a graph showing the relationship between codes and output impedance;

FIG. 9 is a graph showing the results of simulation using SPICE;

25 FIG. 10 is a diagram showing an example of a code control circuit and an impedance dummy resistor;

FIG. 11 is a diagram showing waveforms observed

during impedance adjustment;

FIG. 12 is an impedance trimming circuit according to a second embodiment;

5 FIG. 13 is an impedance trimming circuit according to a third embodiment;

FIG. 14 is a graph showing the relationship between codes and output impedance according to a fourth embodiment;

10 FIG. 15 is a diagram showing an impedance trimming circuit according to a fifth embodiment;

FIG. 16 is a graph showing the relationship between codes and the resistance value of an impedance dummy resistor;

15 FIG. 17 is a graph showing the relationship between the codes and the resistance value of the impedance dummy resistor;

FIG. 18 is a timing chart of the operation of the circuit shown in FIG. 7;

20 FIG. 19 is a view showing an impedance trimming circuit as a reference example;

FIG. 20 is a timing chart of the operation of the circuit shown in FIG. 19;

FIG. 21 is a timing chart of the operation of the circuit in FIG. 19;

25 FIG. 22 is a view showing the output impedance trimming circuit according to the ninth embodiment;

FIG. 23 is a view showing an example of a code

flattening circuit;

FIG. 24 is a timing chart of the operation of the circuit shown in FIG. 22;

5 FIG. 25 is a timing chart of the operation of the circuit in FIG. 22;

FIG. 26 is a timing chart of the operation of the circuit in FIG. 22;

FIG. 27 is a timing chart of the operation of the circuit in FIG. 22;

10 FIG. 28 is a view showing the input impedance trimming circuit according to the ninth embodiment;

FIG. 29 is a view showing the input/output impedance trimming circuit according to the ninth embodiment;

15 FIG. 30 is a view showing base elements in the impedance trimming circuit according to an example of the present invention; and

20 FIG. 31 is a view showing base elements in the impedance trimming circuit according to another example of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

With reference to the drawings, description will be given of an impedance trimming circuit according to an example of the present invention.

25 1. Outline

First, the impedance trimming circuit according to the example of the present invention has a common bias

5 circuit composed of a reference voltage circuit, an internal resistor R1, an accurate external resistor Rext, and an operational amplifier OP1, and an output impedance trimming circuit composed of another internal resistor Rto, a driver dummy resistor Rdrv, an output impedance dummy resistor Rto_trim, an operational amplifier OP1, a comparator CMP, and a code control circuit.

10 The following definitions are assumed: the resistance value of the internal resistor is defined as R1, the resistance value of the accurate external resistor is defined as Rext, the resistance value of the second internal resistor is defined as Rto, the resistance value of the driver dummy resistor is defined as Rdrv, and the resistance value of the output impedance dummy resistor is defined as Rto_trim. Then, the value Rto_trim is switched so as to establish the relationship shown below or the relationship closest to it.

15
$$\text{Rext} : \text{R1} = (\text{Rdrv} + \text{Rto_trim}) : \text{Rto}$$

20 Then, a driver circuit is allowed to reflect this switching information.

25 The impedance trimming circuit according to the example of the present invention further has an input impedance trimming circuit composed of another internal resistor Rti, an input impedance dummy resistor Rto_trim, an operational amplifier OP2, a comparator

CMP, and a code control circuit. A resistance value of this third internal resistor is defined as R_{ti} , and the resistance value of the input impedance dummy resistor is defined as R_{ti_trim} . Then, the value R_{ti_trim} is 5 switched so as to establish the relationship shown below or a relationship closest to it.

$$R_{ext} : R_1 = R_{ti_trim} : R_{ti}$$

Then, an input impedance circuit is allowed to reflect this switching information

10 The impedance trimming circuit has only to have at least one of the output impedance trimming circuit and the input impedance trimming circuit. Further, if only the output impedance trimming circuit or input impedance trimming circuit is used or if both impedance 15 trimming circuits are used, a plurality of impedance trimming circuits of each type may be present.

2. First Embodiment

FIG. 7 shows an impedance trimming circuit according to a first embodiment of the present 20 invention.

Reference character R_{drv} (symbol Δ) denotes an output driver. A common bias section 11 has the internal resistor R_1 and accurate external resistor R_{ext} connected together via a node V_{r1} , the operational 25 amplifier OP_1 to which an internal reference voltage V_{ref} and the voltage at the node V_{r1} are inputted, a P channel MOS transistor P_1 , and an N channel MOS

transistor N1. The P channel MOS transistor P1, connected to a power source VDD, is a bias generating circuit used to generate a small-current bias provided to another circuit. This is an accessory circuit.

5 Operations of this circuit will be described below with reference to FIG. 7.

10 The operational amplifier OP1 controls a gate voltage of the N channel MOS transistor (current control element) N1 so that the voltage Vr1 equals the internal reference voltage Vref. The voltage Vr2 is the voltage Vr1 plus a voltage drop at the resistor R1 with a current I1, i.e. $Vr2 = Vr1 + (R1/Rext) \times Vr1$.

A specific example of calculation will be shown below.

15 The internal reference voltage Vref is assumed to be, for example, $1.2 \text{ V} \pm 5\%$. The external resistor Rext is assumed to offer an accurate resistance of, for example, $12 \text{ k}\Omega \pm 0.1\%$. The power voltage VDD is assumed to be, for example, $3.3 \text{ V} \pm 10\%$. The offset voltage at the operational amplifier OP1 is assumed to be, for example, $\pm 10 \text{ mV}$.

20 A negative feedback circuit composed of the operational amplifier OP1 and the N channel MOS transistor (current control element) N1 operates to make a value for a voltage drop at the external resistor Rext equal to the internal reference voltage Vref. As a result, Vr1 becomes Vref. The accuracy is

(1.2 V \pm 5%) \pm 10 mV, i.e. 1.2 V \pm 0.07 V owing to the effects of a variation in internal reference voltage V_{ref} and the offset voltage at the operational amplifier OP1.

5 The current I_1 is equal to V_{r1}/R_{ext} . The current I_1 also varies and is within the range of, for example, 100 μ A \pm 7 μ A. A voltage V_{r2} is affected directly by a variation in a value for the internal resistor R_1 .
10 If the variation in the value for the internal resistor R_1 is, for example, 2.4 k Ω \pm 20%, then the voltage V_{r2} is given as follows:

$$\begin{aligned} V_{r2} &= V_{r1} + I_1 \times R_1 \\ &= (1.2V \pm 0.07V) + (100\mu A \pm 7\mu A) \times (2.4k\Omega \pm 0.48k\Omega) \\ &= 1.44V \pm 0.13V \end{aligned}$$

15 Importantly, the voltage V_{r2} corresponds to the detection of a ratio containing a difference in resistance value between the internal resistor R_1 and the external resistor R_{ext} .

20 Now, description will be given of an output impedance trimming section 12.

The output impedance trimming section is composed of the comparator CMP to which the voltage V_{r1} and a voltage V_{t01} are inputted, an operational amplifier OP2 to which the voltage V_{r2} and a voltage V_{t02} are inputted, a code control circuit 13 that receives an output signal from the comparator CMP, an N channel MOS transistor (current control element) N2, the internal

resistor Rto, the output impedance dummy resistor Rto_trim, and the output driver dummy resistor Rdrv.

The operational amplifier OP2 controls a gate voltage of the N channel MOS transistor N2 so that 5 the voltage Vto2 equals the voltage Vr2. In this condition, the voltage Vto1 is divided into Rto and (Rto_trim + Rdrv). However, importantly, the ratio of Rext to R1 is equal to the ratio of Rto_trim + Rdrv to Rto.

10 $R_{ext} : R_1 = (R_{to_trim} + R_{drv}) : R_{to}$

The value for the external resistor Rext is accurate. Thus, even if the value for the internal resistor R1, Rto, Rto_trim, or Rdrv varies, the value Rto_trim + Rdrv can generally be accurately brought 15 into the range of a standard value by manufacturing a circuit so that R1 and Rto have a good relative accuracy.

The code control circuit 13 is composed of, for example, a multistage shift register. An output from 20 the comparator CMP, a result of a comparison of Vr1 with Vto1, is inputted to the multistage shift register that carries out a shifting operation on the basis of a clock signal CLK. A code is obtained from each stage of the shift register to switch among the resistors. 25 To switch among the resistors, it is possible to use, for example, the circuit shown in the second example of the prior art.

Then, as the clock signal CLK is supplied many times, the state is established where the relationship between the potentials V_{r1} and V_{t01} exhibits the most frequent switching between a positive side and a negative side, i.e. the potentials V_{r1} and V_{t01} have the closest values that vary between the positive side and the negative side or where the code is stopped and stabilized. This state corresponds to a code with which the value $R_{t0_trim} + R_{drv}$ is closest to the standard.

A specific example of a calculation will be shown below.

If the offset voltage at the operational amplifier is, for example, ± 10 mV, then the following equation is given;

$$\begin{aligned} V_{t02} &= V_{r2} \pm 10 \text{ mV} = 1.44 \text{ V} \pm 0.13 \text{ V} \pm 10 \text{ mV} \\ &= 1.44 \text{ V} \pm 0.14 \text{ V} \end{aligned}$$

A current value I_{t0} is equal to $V_{t02} / (R_{t0} + R_{t0_trim} + R_{drv})$.

Because of the current I_{t0} , V_{t01} has the following voltage effects:

$$V_{t01} = I_{t0} \times (R_{t0_trim} + R_{drv})$$

Consequently, the following equation is established:

$$\begin{aligned} V_{t01} &= V_{t02} / (R_{t0} + R_{t0_trim} + R_{drv}) \times (R_{t0_trim} + R_{drv}) \\ &= V_{t02} / (1 + R_{t0} / (R_{t0_trim} + R_{drv})) \end{aligned}$$

V_{t02} is determined by the ratio of V_{t02} to

resistance.

The comparator CMP selects R_{to_trim} so that V_{rl} is closest to V_{tol} . Accordingly, on this occasion, if the offset voltage at the comparator CMP is defined as V_{offcmp} (± 20 mV), then the following equation is given:

$$V_{tol} = V_{rl} \pm V_{offcmp}$$

Specifically, the right

$$side = 1.2 \text{ V} \pm 0.07 \text{ V} \pm 0.02 \text{ V} = 1.2 \text{ V} \pm 0.09 \text{ V}.$$

If the right side equals the left side V_{tol} , then the following equation is established:

$$1.2V \pm 0.09V = (1.44V \pm 0.14V) / (1 + R_{to} / (R_{to_trim} + R_{drv}))$$

Here, it is assumed that the output impedance trimming circuit composed of R_{to} and $(R_{to_trim} + R_{drv})$ offers resistance that is, for example, six times as large as that of an actual output buffer circuit in order to reduce current consumption. Accordingly, if an actual driver output impedance is to be 45Ω , then $R_{to_trim} + R_{drv}$ is 270Ω .

R_{to} is 54Ω on the basis of the relationship

$$R_{ext}:R_1 = (R_{to_trim} + R_{drv}):R_{to}, \text{ i.e. } 12 \text{ K}\Omega:2.4 \text{ K} = 270\Omega:54\Omega.$$

Further, it is assumed that $R_{to_rim} + R_{drv} = 270\Omega$, $R_{to_trim} = 240\Omega$, and $R_{drv} = 30\Omega$.

Importantly, the resistors R_1 and R_{to} are formed within the same integrated circuit and can thus be manufactured so as to have a good relative accuracy.

Further, the resistor R_{to_trim} can also be manufactured

so as to have a good relative accuracy. However, since the resistor Rdrv is composed of, for example, a MOS transistor, its variation contains a variation associated with the manufacture of the transistor.

5 This is substituted into the previous equation.

$$1.2V \pm 0.09V = (1.44V \pm 0.14V) / (1 + (Rto / (Rto_trim + Rdrv)))$$

Then, the following equation is established:

$$\begin{aligned} Rto / (Rto_trim + Rdrv) \\ = ((1.44V \pm 0.14V) / (1.2V \pm 0.09V)) - 1 \end{aligned}$$

10 Accordingly, the adjusted resistance value

Rto_trim is written on the left side, the following equation is given:

$$Rto_trim = (Rto / ((1.44V \pm 0.14V) / (1.2V \pm 0.09V)) - 1) - Rdrv$$

15 Specific values are substituted into the above equations.

If the following assumptions are made:

$$Rdrv = 30\Omega \pm 20\Omega,$$

$$Rto = 54\Omega \pm 10.8\Omega$$

then the following equation is given:

20

$$\begin{aligned} Rto_trim = ((54\Omega \pm 10.8\Omega) / ((1.44V \pm 0.14V) \\ / (1.2V \pm 0.09V) - 1)) - (30\Omega \pm 20\Omega) \end{aligned}$$

If a center condition is used for all cases, then the following calculation can be executed:

$$\begin{aligned} Rto_trim(\text{center}) &= (54\Omega / ((1.44V / 1.2V) - 1)) - 30\Omega \\ &= 240\Omega \end{aligned}$$

That is, if Rto_trim is adjusted to be closest to 240Ω , the final value is determined to be 240Ω .

If the value for the resistor R_{drv} connected in series with the resistor R_{to_trim} is added to this final value, then $30\Omega + 240\Omega = 270\Omega$. Thus, the resistance is accurately adjusted to a value that is six times as large as the target one, i.e. 45Ω .

Variations in various factors can be determined using the above calculation. However, this requires various calculations and their description is thus omitted. An important point is that a wide range of variation is assumed so that the value for the output impedance dummy resistor R_{to_trim} can be adjusted over a wide range.

FIG. 8 shows an example of an adjustment range for the trimming circuit.

Actually, under the same conditions as those for the driver circuit, too large a current may flow. Thus, to limit the current, the value for the output impedance dummy resistor R_{to_trim} is designed to be about six times as large as the target value. Table 1, shown below, shows this value in terms of the impedance of the output driver.

Table 1

Rtrm	53.33	*0.8	*1.2	*0.9	*1.1
Rsw	5	3	8	3	8
Code	Typ	(-20%)	(+20%)	(-10%)	(+10%)
0	58.33	45.67	72.00	51.00	66.67
1	53.70	41.96	66.43	46.83	61.57
2	40.80	38.84	61.76	43.32	57.28
3	46.48	36.19	57.78	40.33	53.63
4	43.62	33.90	54.34	37.76	50.48
5	41.13	31.90	51.35	35.53	47.74
6	38.94	30.15	48.73	33.55	45.33
7	37.00	28.60	46.40	31.80	43.20

5 This table shows how the output impedance of the actual driver varies when the code control circuit 13 is switched among eight states obtained by constructing the code control circuit 13 using a 7-stage shift register.

10 This graph contains the range of a variation and is based on the assumptions that R_{to_trim} is 20% and that a switch required for switching operations offers resistance $5\Omega + 3\Omega / -2\Omega$.

15 For calculations, it is assumed that the resistance value of each switch = 5Ω , $R_1, \dots, R_7 = 560\Omega$, and the driver resistance $R_{drv} = 5\Omega$.

20 In consideration of a variation in the value for the internal resistor, $R_{to_trim} + R_{drv}$ is set so as to be arbitrarily switched within a certain range around a target value (in this case, 45Ω) using codes.

For example, for the driver circuit, $R_{to} + R_{drv}$ is set to be 58.33Ω at maximum and 37Ω at minimum. Cases indicated by *0.8 and *1.2 are examples of calculations that take various variations or dependencies into consideration. Under a standard condition, the optimum value of 45Ω lies between codes 3 and 4. However, under the best condition indicated by *0.8, the optimum value is found between codes 0 and 1. Under the worst condition indicated by *1.2, the optimum value is found between codes 6 and 7.

It is evident that even if the standard value is set at $45\Omega \pm 5\Omega$, the value can be adjusted even with a variation of $\pm 20\%$ in the value for the internal resistor.

Consequently, $V_{t1} \neq V_{t02}$, I_{to} , and others are controlled so that V_{r1} equals V_{t01} . Therefore, the values including V_{ref} are only intermediate variables for a control system the final result of which is an accurate resistance ratio. It is thus evident that direct effects have been eliminated.

Furthermore, importantly, although not shown in detail, the present circuit is very insensitive to V_{ref} , the offset voltage at the operational amplifier OP1, a variation in current, and the like. The resistance ratio of R_1 to R_{to} must be accurate, but a relative accuracy of $\pm 0.5\%$ or less can be easily accomplished by arranging these resistors so as to

occupy a certain area or larger in the LSI and to lie close to each other.

FIG. 9 shows the results of circuit simulation using SPICE except for the impedance trimming circuit 5 Rtrim.

In this figure, the axis of ordinate indicates Vtol to Vrl, an input to the comparator CMP, while the axis of abscissa indicates the elapsed time from 0 to 10 μ s. This figure shows the results of simulation 10 obtained by linearly varying the value Rtrim. Even if the ranges of variations described above are combined together 100 times using a Monte Carlo method, all 20 lines other than the lower two cross a 0-V line. This indicates the possibility of adjustment.

FIG. 10 shows an embodiment of the control circuit and impedance dummy resistor.

A code control circuit 13 comprises, e.g., a seven-stage shift register. An impedance dummy resistor Rto trim comprises a resistor R1 and seven 20 series elements connected in parallel with the resistor R1. Each of the series elements comprises a resistor R and a switch SW.

It should be noted that the resistance values of the resistors R and R1 are denoted by Rtrm. Also, the 25 resistance values of the resistors R and R1 which are measured when the respective switches are turned on are denoted by Rsw. The following explanation will be

given on the supposition that R_{SW} is 0.

In this embodiment, the number of code control signals (code values) is eight. For example, they are 0 to 7. To be more specific, when all the output signals a, b, ... g of the code control circuit 13 are "L" (= "0"), e.g., the code value is 0, all the switches SW are turned off, and the resistance value of the impedance dummy resistor $R_{TO\ TRIM}$ is equal to R_{TRIM} .

When one of the output signals a, b, ... g of the code control circuit 13 is "H" (= "1"), e.g., the code value is 1, one of the switches SW is turned on, and the resistance value of the impedance dummy resistor $R_{TO\ TRIM}$ is $R_{TRIM}/2$.

In such a manner, with respect to the output signals a, b, ... g of the code control circuit 13, the impedance dummy resistor $R_{TO\ TRIM}$ varies within a range from R_{TRIM} to $R_{TRIM}/(K+1)$ in accordance with the number of signals indicating "1".

In the circuit according to the above embodiment, when $V_{TOL} > V_{RL}$, the comparator shown in FIG. 1 continuously outputs "1". The output "1" from a comparator CMP synchronizes with a clock signal CLK. The stages of the shift registers successively receive the output "1". That is, when $V_{TOL} > V_{RL}$, the number of those of the output signals a, b, ... g of the code control circuit 13, which indicate "1", increases by degrees.

To be more specific, the code value increases by degrees, the number of switches SW which are in the ON state increases by degrees, and the resistance value of the impedance dummy resistor R_{to trim} lowers by 5 degrees.

On the other hand, when $V_{tol} < V_{rl}$, the comparator in FIG. 1 outputs "0". The output "0" synchronizes with the clock signal CLK. The stages of the shift register successively receives the output "0". Then, 10 when a predetermined time period lapses, and "1" input to the first stage of the shift register is output from the last stage thereof, the code value decreases, the number of switches SW which are in the ON state decreases, and the resistance value of the impedance 15 dummy resistor R_{to trim} increases.

Thereafter, the code value repeatedly varies between a value at which " $V_{tol} > V_{rl}$ " is satisfied and a value at which " $V_{tol} < V_{rl}$ " is satisfied (periodic variation). This applies to a case where the code 20 value varies by a 1-bit width (between two values). In a case where the code value varies by a two-bit width (between three values), it repeatedly varies between a value at which " $V_{tol} \geq V_{rl}$ " is satisfied and a value at which " $V_{tol} \leq V_{rl}$ " is satisfied.

25 In the above manner, the code value is set to be optimal. When all the values of the stages of the shift register are "1", i.e., all the resistors R₁ are

electrically connected in parallel, and then when
5 $V_{tol} \geq V_{rl}$, the code value is determined in this state
(it is set at the maximum value "7"). When all the
values of the stages of the shift register are "0",
when $V_{tol} \leq V_{rl}$, the code value is determined in this
state (it is set at the minimum value "0").

10 The operational waveform diagram in FIG. 11
indicates this adjustment.

This figure shows how the state changes.

3. Second Embodiment

15 FIG. 12 shows an impedance trimming circuit
according to a second embodiment of the present
invention.

This embodiment relates to an input impedance
trimming circuit 14. Compared to the above output
impedance trimming circuit, this circuit does not
require any driver dummy resistors or drivers but
simply trims resistance and uses the code obtained to
20 adjust the input impedance.

Operations of this circuit are the same as those
in the first embodiment. Their description is thus
omitted.

25 4. Third Embodiment

FIG. 13 shows an impedance trimming circuit
according to a third embodiment of the present

invention.

This embodiment relates to an I/O impedance trimming circuit. This circuit has the output impedance trimming section 12 and the input impedance trimming section 14. In this case, a single common bias section 11 can be shared by the output impedance trimming section 12 and the input impedance trimming section 14.

Operations of this circuit are the same as those in the first embodiment. Their description is thus omitted.

5. Fourth Embodiment

FIG. 14 shows an impedance trimming circuit according to a fourth embodiment of the present invention.

This embodiment relates to a resistance adjustment circuit.

With the method shown in the second example of the prior art, the impedance is adjusted by connecting the resistor R0 in parallel with the resistors R1 to R8 having the same resistance value as the resistor R0. However, this method is disadvantageous in that the number of code increases with the allowable variation range and that it is necessary to switch the resistance over a wide range from smaller to larger resistance.

In this embodiment, the relationship between the code and the resistance value is represented by

an S-shaped curve or a polygonal line. Accordingly, even with a wide range of variation, the impedance can be adjusted using a small number of codes.

Specifically, for example, in the second example 5 of the prior art, the value for the resistor R0 is set at 55Ω . The value for the resistors R1 and R2 is set at 67Ω . The value for the resistors R3, R4, and R5 is set at 100Ω . The value for the resistor R6 is set at 42Ω . The value for the resistor R7 is set at 33Ω .
10 In this manner, the different resistance values are used for the respective resistors so that the relationship between the code and the resistance value is represented by an S-shaped curve or a polygonal line.

15 In this regard, a decode circuit may be provided which serves to change the resistance values used for adjustment. Rather than using simple shift registers for switch control, this decode circuit detects the number of level 1 on the basis of an output from each 20 stage of the multistage shift register, to select resistors to be connected in parallel on the basis of this number.

6. Fifth Embodiment

FIG. 15 shows an impedance trimming circuit 25 according to a fifth embodiment of the present invention.

This embodiment relates to a resistance adjustment

circuit and is an applied example of the resistance adjustment shown in the first embodiment.

The LSI has the following parasitic resistances: lead frame resistance, bonding wire resistance, intra-pellet wiring resistance, and the like, which are parasitic on a package. Thus, from the outside of the package, the impedance of the LSI appears like a series connection of all these resistances. In this embodiment, all these parasitic resistances are estimated before the value for the impedance dummy resistor R_{trim} is adjusted. Then, the impedance is adjusted to exhibit a desired value with all parasitic resistances present.

For example, if wiring resistance R_{metal} is 0.5Ω , bonding wire resistance R_{bdg} is 0.3Ω , and lead frame resistance R_{frm} is 0.2Ω , then the resistance of the whole current path from power pin to output pin of the buffer is $2 \times (0.5\Omega + 0.3\Omega + 0.2\Omega) = 2\Omega$.

In such a case, the impedance dummy resistance R_{trim} may be adjusted to a value smaller than the desired resistance value, 45Ω , by about 2Ω , i.e. 43Ω . However, with the present circuit, it is cumbersome to switch the value for the impedance dummy resistor R_{trim} around this value, 43Ω .

In this embodiment, the adjustment range of the value for the impedance dummy resistor R_{trim} can be shifted by switching the value for the resistor R_1 .

If $R_{ext}:R_1 = R_{trim}:R_t$ and R_{trim} is to be changed from 45Ω to 43Ω for adjustment, the value R_1 may be increased by a value of $45/43$. In this case, to allow the value R_1 to be switched with all expected parasitic resistances taken into account, an LSI pattern may be provided before the value R_1 is increased or reduced.

5 A switching operation may be performed by using an analog switch, switching the metal layer using a master slice, or using other methods.

10 FIGS. 16 and 17 show an example of a variation in resistance with respect to the code observed if the value for the impedance dummy resistor R_{trim} is switched with the parasitic resistances taken into account.

15 As shown in these figures, if the parasitic resistances are small, the value for the impedance dummy resistor R_{trim} can be switched around a larger value, e.g. 43Ω . On the other hand, if the parasitic resistances are large, the value for the impedance dummy resistor R_{trim} can be switched around a smaller value, e.g. 40Ω .

20

Even with a different package, the impedance can be kept constant according to this embodiment.

7. Sixth Embodiment

25 Now, description will be given of an impedance trimming circuit according to a sixth embodiment of the present invention.

This embodiment is a variation of the above described fifth embodiment. Specifically, in FIG. 15, the value for the accurate resistor R_{ext} need not necessarily be singular. For example, if the accurate resistor R_{ext} has a resistance value of $12 \text{ k}\Omega$, the value for the resistor R_1 is set at $2.4 \text{ k}\Omega$. On the other hand, if the accurate resistor R_{ext} has a resistance value of $13 \text{ k}\Omega$, the value for the resistor R_1 , $2.4 \text{ k}\Omega$, may be increased by $(13/12) \times 2.4 \text{ k}\Omega$ up to $2.6 \text{ k}\Omega$.

Operations of this circuit are omitted, but the relationship $R_{ext}:R_1 = R_{trim}:R_t$ is maintained.

Thus, the impedance can be kept constant even with a change in the value for the accurate resistor R_{ext} .

15 8. Seventh Embodiment

Now, description will be given of an impedance trimming circuit according to a seventh embodiment of the present invention.

This embodiment is a combination of the above described fifth and sixth embodiments. When the fifth and sixth embodiments are thus combined together, the resistance value of the resistor R_1 can be switched to correct the resistance value of the accurate resistor R_{ext} and the values for various resistances parasitic on the package. That is, the impedance can be kept constant even with a change in the value for the accurate resistor R_{ext} or in the type of the package.

9. Eighth Embodiment

Now, description will be given of an impedance trimming circuit according to an eighth embodiment of the present invention.

5 This embodiment relates to measures taken if the internal reference voltage V_{ref} deviates from the desired value in the above described fifth embodiment. For example, it is assumed that the target value for the internal reference value is 1.2 V and that the 10 value for the accurate resistor R_{ext} is $12 \text{ k}\Omega$. In this case, a current flowing through the accurate resistor R_{ext} is $V_{ref}/R_{ext} = 100 \mu\text{A}$.

15 Here, the internal reference voltage V_{ref} may deviate from 1.2 V owing to a change in manufacturing process or the like. If the internal power voltage V_{ref} becomes 1.25 V, then a current of $125 \mu\text{A}$ flows through the accurate resistor R_{ext} . The voltage V_{r2} also increases with a voltage drop at the resistor R_1 .

20 In such a case, the resistor R_1 is divided into two parts, and the midpoint between these parts is defined as V_{r1} and connected to a negative input terminal of the operational amplifier OP_1 . Then, a potential difference of $1.25 \text{ V} - 1.2 \text{ V} = 0.05$ is absorbed by one (the lower part of R_1) of the two parts 25 which is connected to the accurate resistor R_{ext} . Further, the other part (the upper part of R_1) connected to an output terminal of the operational

amplifier OP1 has a resistance value that meets the relationship $R_{ext} : (\text{lower part of } R_1 + \text{upper part of } R_1) = R_{trim} : R_t$.

5 Thus, according to the present embodiment, even with a variation in internal reference voltage V_{ref} , the operational current can be kept constant.

Therefore, the value R_{trim} can be accurately adjusted.

10. Ninth Embodiment

10 The impedance trimming circuit according to the ninth embodiment of the present application will be explained.

(1) The impedance trimming circuit according to the ninth embodiment is provided based on the following premise:

15 The above impedance trimming circuits according to the first to eighth embodiments execute impedance matching with respect to the output impedance, input impedance, terminal resistance or the like, to thereby suppress reflection of signals, thus allowing serial 20 signals to be transferred at a high speed while maintaining their high quality, and automatically perform such trimming at a high accuracy.

25 However, for example, the output impedance trimming circuit shown in FIG. 7 performs trimming of the output impedance, with the output signal of the code control circuit 13 kept as it is. Thus, shown in FIG. 18, when V_{t01} becomes close to V_{rl} , it repeatedly

increases and decreases with respect to V_{r1} .

As a result, the value of the impedance dummy resistor R_{to} trim of the output impedance trimming circuit in FIG. 7 continuously varies during trimming of the output impedance. This variation may affect the 5 operation of the circuit.

Similarly, for example, the input impedance trimming circuit shown in FIG. 12 performs trimming of the input impedance, with the output signal of the code 10 control signal 13 kept as it is. Thus, the same phenomenon as in the circuit in FIG. 18 occurs. That is, V_{t1} does not constantly vary. As a result, the value of the input impedance dummy resistor R_{ti} trim of the input impedance trimming circuit in FIG. 12 also 15 continuously varies during trimming of the input impedance.

Furthermore, shown in FIG. 18, when V_{t01} varies by a two-bit width with respect to V_{r1} , e.g., V_{t01} varies between "2" and "4", it is closest to V_{r1} when 20 it is "3". Thus, in such a case, trimming can be executed at a high accuracy by fixing the code value which controls the impedance, at a value at which V_{t01} is "3", i.e., the central value of the variation range of V_{t01} . The same is true of V_{t1} .

25 It can be therefore found by considering the above that when V_{t01} or V_{t1} reaches a value close to V_{r1} which is a target value, it is appropriate that the

input and output impedance dummy resistors R_{to} trim and R_{ti} trim be fixed at predetermined values, i.e., the output signal of the code control signal 13 be fixed at a predetermined value.

5 Then, it should be noted that, for example, the impedance trimming circuit disclosed in patent document 2 (Jpn. Pat. Appln. KOKAI Publication No. 2003-69412) is used as an impedance trimming circuit which latches the value of the output signal of a code control 10 circuit.

FIG. 19 shows a main portion of the impedance trimming circuit disclosed in patent document 2. The points of this circuit will be described below, but its detailed explanation will be omitted.

15 The first point of the impedance trimming circuit in patent document 2 resides in that trimming of the impedance is carried out without using an external resistor by a current source 215 provided in a chip, unlike the impedance trimming circuit of the present 20 invention. The second point of the impedance trimming circuit of patent document 2 resides in that when V_{target} reaches to a value close to C_{ref} , a thermal code C_{1i} corresponding to the code of the impedance trimming circuit of the present invention is fixed.

25 However, in the impedance trimming circuit of patent document 2, when V_{target} is greater than V_{ref} as shown in, e.g., a timing chart of FIG. 20, a U/D signal

becomes "H", and when the number of times V_{target} exceeds V_{ref} reaches two, i.e., the U/D signal becomes "H" twice, the time at which the U/D signal varies from "H" to "L" after becoming "H" twice is detected by a control circuit 211, and then a signal COMPLETE is set at "H", and the value of the thermal code C_{li} is fixed. Thus, when the signal COMPLETE is set at "H", V_{target} does not coincide with the central value (V_{ref}) of its variation range, as a result of which trimming cannot be performed with a high accuracy.

Therefore, the impedance trimming circuit according to the ninth embodiment, which will be explained below, fixes a code value for use in impedance trimming at a high speed at a value at which V_{t01} or V_{t11} is closest to V_{r1} ($V_{t01} = V_{r1}$ or $V_{t11} = V_{r1}$ if V_{t01} or V_{t11} varies by a two-bit width with respect to V_{ref}), when V_{t01} or V_{t11} reaches a value close to V_{t11} which is a target value.

(2) Example 1

FIG. 22 shows example 1 of the impedance trimming circuit according to the ninth embodiment of the present invention.

R_{drv} (symbol Δ) denotes an output driver.

A common bias section 11 includes an internal variable resistor R_{1a} connected via a node V_{r1} , a precision external resistor R_{ext} , an operational amplifier $OP1$ to which an internal reference voltage

Vref and a voltage of the node Vr1 are to be applied, P-channel MOS transistors P1a and P1b, and an N-channel MOS transistor N1. The P-channel MOS transistor P1a and P1b are connected to a power supply VDD. These 5 transistors are bias generating circuits for generating a constant-current bias, and also accessory circuits.

Explanations for the operation of the common bias section 11 and an example of the operation will be omitted, since they are the same as those of the common 10 bias section shown in FIG. 7.

The output impedance trimming section 12 comprises a comparator CMP to which voltages Vr1 and Vt01 are to be applied, an operational amplifier OP2 to which voltages Vr1 and Vt02 are to be applied, a code control 15 circuit 13 which receives the output signal of the comparator CMP, an N-channel MOS transistor (current control element) N2, an internal resistor Rto, an output impedance dummy resistor Rto trim, and an output driver dummy resistor Rdrv.

The operational amplifier OP2 controls the gate voltage of the N-channel MOS transistor N2 such that the voltage Vt02 is equal to the voltage Vr2. In this state, the voltage Vt01 is determined by the ratio between resistors Rto and Rto trim + Rdrv. It is 25 important that the ratio of Rext to R1 is equal to that of Rto trim + Rdrv to Rto. That is:

$$R_{ext}: R1 = (R_{to\ trim} + R_{drv}): R_{to}$$

The external resistor R_{ext} is highly accurate. Thus, even if the manufactured output impedance trimming sections are variant with respect to each of the resistors R_1 , R_{to} , $R_{to\ trim}$ and R_{drv} , 5 in general, if the relative precision between the internal resistors R_1 and R_{to} is high, the value of $R_{to\ trim} + R_{drv}$ can be made to fall within a standard range.

10 The code control circuit 13 comprises, e.g., a multistage shift register in which the code value varies in response to a clock signal CLK. The output of the comparator CMP which is obtained as a result of comparison between V_{rl} and V_{tol} is input to the multi-stage shift register. The figures of the code value 15 are taken out from the respective stages of the shift register, and turning on/off of the resistors is switched. In order to switch turning on/off of the resistor, the second example of the prior art can be used.

20 V_{tol} varies by degrees to reach V_{rl} provided as a target value, in synchronism with the clock signal CLK. Then, when the relationship between V_{rl} and V_{tol} repeatedly varies, i.e., V_{tol} increases and decreases with respect to V_{rl} , the code control circuit 13 25 outputs a code value at which $R_{to\ trim} + R_{drv}$ is closest to the standard value.

Explanations for the operation of the output

impedance trimming section 12 and an example of the operation will be omitted, since they are not greatly different from those of the output impedance trimming section shown in FIG. 7.

5 A code flattening section 15 includes a code flattening circuit 16.

The code flattening circuit 16 receives the output signal (code value) of the code control circuit 13. The code flattening circuit 16 outputs the output signal of the code control circuit 13 as an output signal SEL, as it is, when V_{t01} always varies in one direction (e.g., plus direction) toward V_{r1} . Then, when V_{t01} is closest to V_{r1} , the code flattening circuit 16 fixes the output signal (code value) of the code control circuit 13 at a value at which V_{t01} is closest to V_{r1} , and thereafter outputs the fixed code value as the output signal SEL.

FIG. 23 shows an example of the code flattening circuit.

20 A register 17 latches a code control signal (code value) output from the code control circuit 13 shown in FIG. 22. To the register 17, a down detection signal DOWN is input. When the down detection signal DOWN becomes "H", the register 17 latches the code control signal.

25 A down detection signal generating circuit 18 synchronizes with the clock signal CLK, fetches

an up/down signal UP/DOWN, which is disclosed in, e.g., FIG. 10, and outputs the down detection signal DOWN on the basis of the up/down signal UP/DOWN.

5 The example shown in FIG. 10 has the following circuit structure: when V_{tol} is greater than V_{rl} , the up/down signal UP/DOWN becomes "H" (= "1"), and when V_{tol} is smaller than V_{rl} , the up/down signal UP/DOWN becomes "L" (= "0").

10 In the example of FIGS. 22 and 23, it is considered that V_{tol} gradually increases from a condition satisfying $V_{tol} < V_{rl}$. Thus, in those examples, the example of FIG. 10 is modified to achieve the following circuit structure: when V_{tol} is smaller than V_{rl} , the up/down signal UP/DOWN becomes "H" (= "1"), and when V_{tol} is greater than V_{rl} , the up/down signal UP/DOWN becomes "L" (= "0"). Such a circuit structure can be easily achieved by modifying the comparator CMP.

15

20 In example 1, the up/down signal UP/DOWN becomes "H" (UP) when V_{tol} is smaller than V_{rl} . This indicates that V_{tol} increases toward V_{rl} , and thus the down detection signal is kept "L".

25 On the other hand, the up/down signal UP/DOWN becomes "L" (DOWN) when V_{tol} is greater than V_{rl} . This indicates that V_{tol} exceeds V_{rl} . Thereafter, since V_{tol} needs to be decreased, the down detection signal DOWN is made to be "H".

Suppose that at the time of impedance trimming, Vtol increases by degrees toward Vrl, i.e., the target value, as stated above.

Needless to say, as a modification, suppose that
5 Vtol gradually decreases toward Vrl (target value), an up detection signal generating circuit for detecting that Vtol increases may be provided as a modification of the down detection signal generating circuit 18. (In this case, the structure in FIG. 10 can be used as
10 it is).

A multiplexor (MUX) 19 selects and outputs one of the output signal (code control signal) of the code control circuit 13 and the output signal of the register 17, which are shown in FIG. 22.

15 To be more specific, when the down detection signal DOWN is "L", the multiplexor (MUX) 19 selects and outputs the output signal (code control signal) of the code control circuit in FIG. 22. When the down detection signal DOWN is "H", the multiplexor (MUX) 19
20 selects and outputs the output signal of the register 17.

That is, once the down detection signal DOWN becomes "H", the multiplexor (MUX) 19 necessarily selects and outputs the output signal of the register 17.

25 A bit variation monitoring circuit 20 always monitors the code control signal (code value), i.e.,

a bit value. Then, when the bit value becomes the maximum value (which is "7" in the case where the bit value varies from the range of "0" to "7"), the bit variation monitoring circuit 20 outputs 5 a predetermined value (e.g., "6") as a bit value.

At this time, the bit variation monitoring circuit 20 outputs a control signal CT for use in controlling the operation of a multiplexor (MUX) 21, so that the multiplexor (MUX) 21 selects the output signal of the 10 bit variation monitoring circuit 20.

In general, the bit variation circuit 20 is provided by a user's request. Thus, it may be omitted.

Next, the operation of the output impedance trimming circuit shown in FIGS. 22 and 23 will be 15 explained.

First, the case where V_{t01} periodically increases and decreases with respect to V_{r1} will be explained by referring to the timing chart in FIG. 24.

In the initial state, V_{t01} is far from V_{r1} . Thus, 20 V_{t01} synchronizes with the clock signal CLK, and increases by degrees. In order that the operation be easily understood, in the following explanation, V_{t01} is expressed by "0" to "7" to correspond to the code control signal (the code value of which varies from the 25 range of "0" to "7") output from the code control circuit 13.

Under the above condition, since V_{t01} continuously

increases, the down detection signal generating circuit 18 continuously maintains "L" as the value of, e.g., the down detection signal DOWN. At this time, the register 17 does not latch the code control signal, and 5 the multiplexor (MUX) 19 selects and outputs the code control signal from the code control circuit 13.

Furthermore, since the value of the code control signal is not the maximum value, the bit variation monitoring circuit 20 controls the multiplexor 21 such 10 that the multiplexor 21 selects and outputs the output signal of the multiplexor 19.

When V_{tol} is in the vicinity of V_{rl} , it repeatedly increases and decreases with respect to V_{rl} . For example, in the example of FIG. 24, V_{tol} repeatedly 15 varies between "3" and "4". That is, V_{tol} varies by a 1-bit width with respect to V_{rl} .

The code control circuit 13 outputs "L" (= "0") as the up/down signal UP/DOWN, when V_{tol} varies to be greater than V_{rl} . When the down detection signal 20 generating circuit 18 in the code flattening circuit 16 detects that the up/down signal UP/DOWN becomes "L", it determines that V_{tol} will decrease, and makes the down detection signal DOWN "H".

The down detection signal generating circuit 18 25 may be formed to output the down signal (pulse signal) DOWN, when detecting a down edge of V_{tol} (variation from "4" to "3").

When receiving the first down detection signal DOWN, the register 17 latches "3" as the code control signal, and thereafter, does not accept the input signal. At the same time, the multiplexor 19 selects and outputs the output signal of the register 17, and thereafter, always selects and outputs the output signal of the register 17.

In such a manner, when V_{t01} is in the vicinity of V_{r1} , the code flattening circuit 16 fixes the code control signal (code value) at a value at which V_{t01} is closest to V_{r1} , i.e., "3" in this example. Thus, in precision trimming of the example, the resistance value (code value) of a resistor R_{t0} to use for use in actual trimming of an output impedance can be fixed at an optimal value at a high speed, and thus, it is not necessary to consider the influence of the trimming upon other circuits.

In the example, when V_{t01} is in the vicinity of V_{r1} , and then when it repeatedly increases and decreases with respect to V_{r1} , the output signal (code control signal) SEL of the code flattening circuit 16 is fixed after detection of the first down edge of V_{t01} . In such a manner, the output signal SEL of the code flattening circuit 16 is fixed at an optical value at a high speed.

In the example, when V_{t01} (= "3") < V_{r1} , the output signal (code control signal) SEL of the code

flattening circuit 16 is fixed. However, as shown in the timing chart of FIG. 25, the output signal (code control signal) SEL of the code flattening circuit 16 may be fixed when V_{t01} (= "4") > V_{r1} .

5 Next, the case where V_{t01} periodically increases and decreases by a two-bit length in the vicinity of V_{r1} will be explained with reference to the timing chart of FIG. 26.

10 In the initial state, as stated above, V_{t01} gradually increases in synchronism with the clock signal CLK. Under such a condition, since V_{t01} continuously increases, the down detection signal generating circuit 18 maintains "L" as the value of, e.g., the down detection signal DOWN. At this time, 15 the register 17 does not latch the code control signal, and the multiplexor (MUX) 19 selects and outputs the code control signal from the code control circuit 13.

20 Furthermore, since the value of the code control signal is not the maximum value, the bit variation monitoring section 20 controls the multiplexor 21 such that the multiplexor 21 selects and outputs the output signal of the multiplexor 19.

25 When V_{t01} is in the vicinity of V_{r1} , it repeatedly increases and decreases with respect to V_{r1} . For example, in the example of FIG. 26, V_{t01} varies between "2" and "4", i.e., it varies by a two-bit length with respect to V_{r1} .

The down detection signal generating circuit 18 in the code flattening circuit 16 makes the down detection signal DOWN "H", when detecting that the up/down signal UP/DOWN becomes "L" (DOWN), and then Vt01 decreases.

5 As stated above, the down detection signal generating circuit 18 may be formed to output the down signal (pulse signal) DOWN when detecting a down edge (variation from "4" to "3" and that from "3" to "2") of Vt01.

10 The register 17 latches "3" as the code control signal, when receiving the first down detection signal DOWN, and thereafter, does not accept the input signal. At the same time, the multiplexor 19 selects and outputs the output signal of the register 17, and 15 thereafter always selects and outputs the output signal of the register 17.

20 In such a manner, when Vt01 is in the vicinity of Vr1, the code flattening circuit 16 fixes the code control signal (code value) at a value at which Vt01 is closest to Vr1, i.e., "3" in this example. Thus, in precision trimming of the example, the resistance value (code value) of the resistor R to use for use in actual trimming of an output impedance can be fixed at an optimal value at a high speed, and thus, it is not 25 necessary to consider the influence of the internal circuits upon external circuits.

In the example also, the output signal (code

control signal) SEL of the code flattening circuit 16 is fixed when the first down edge of Vtol is detected. In such a manner, the output signal SEL of the code flattening circuit 16 is fixed at an optimal value at 5 a high speed.

Further, in the example, Vtol varies by a two-bit length with respect to Vrl1. Thus, the code flattening circuit 16 fixes the output signal (code control signal) SEL when Vtol (= "3") = Vrl1. In such a manner, 10 in the example, trimming of the output impedance can be carried out at a high precision.

FIG. 27 shows a timing chart of Vtol which varies with respect to the maximum value "7". At this time, the bit variation monitoring circuit 20 forcibly 15 outputs a predetermined value, which is "6" in this example, as the output signal SEL of the code flattening circuit 16, regardless of the code control signal from the code control circuit 13.

(3) Example 2 of the circuit

FIG. 28 shows example 2 of the impedance trimming circuit according to the ninth embodiment of the 20 present invention.

The impedance trimming circuit provided as example 2 is an input impedance trimming circuit. This 25 circuit does not need the driver dummy resistor or the driver, and merely performs trimming of the resistor, and adjusts the input impedance by using the obtained

code, unlike the above output impedance trimming circuit.

Except the above points, an input impedance trimming circuit 14 does not greatly differ from the output impedance trimming section 12 shown in FIG. 22. Further, a code flattening circuit 16' of a code flattening section 15' is the same as the code flattening circuit 16 of the code flattening section 15 in FIG. 22.

The operation of the above input impedance trimming circuit is the same as that of the impedance trimming circuit according to the first embodiment, and its explanation will be omitted.

(4) Example 3 of the circuit

FIG. 29 shows example 3 of the impedance trimming circuit according to the ninth embodiment of the present invention.

The impedance trimming circuit provided as example 3 is an input/output impedance trimming circuit. This circuit includes an output impedance trimming section 12 and an input impedance trimming section 14. In this case, a common bias section 11 is shared with the input impedance trimming section 12 and the output impedance trimming section 14.

The output impedance trimming section 12 and the code flattening section 15 are the same as the output impedance trimming section 12 and code flattening

section 15 shown in FIG. 22. The input impedance trimming section 14 and the code flattening section 15' are the same as the input impedance trimming section 14 and code flattening section 15' shown in FIG. 28.

5 The operation of the input/output impedance trimming circuit is the same as that of the impedance trimming circuit according to the first embodiment, and its explanation will be omitted.

11. Conclusion

10 As described in the first to eighth embodiments, the following effects are produced by the impedance trimming circuit according to the example of the present invention:

- The circuit can be manufactured using a normal CMOS LSI manufacturing process.
- Only one external resistor is required. This is advantageous in terms of costs.
- The impedance can be kept constant even with a change in the value for the external accurate resistance.
- The impedance can be kept constant even with a change in the layout of the LSI or in parasitic resistance.
- The number of adjustment codes can be easily increased to easily accomplish accurate adjustments.
- The adjustment of the output impedance is also executed on the driver and is thus very accurate.

• The yield can be easily increased in spite of a wider range of variation.

5 • The circuit can be divided into a number of elements. Accordingly, the elements can be easily shared, and the area of the circuit can be reduced.

• The resistance values of the resistor elements used in the LSI can be dynamically determined.

10 • The resistance values of the resistor elements in the LSI can be determined at a high precision, since resistor elements having precision resistance values are provided outside the LSI.

15 • The value (code value) of a code control signal for use in impedance trimming is immediately fixed to an optimal value on the basis of the first down detection signal DOWN. In such a manner, the optimal resistance values of the resistor elements for use in impedance trimming can be determined at a high speed. In addition, thereafter, the determined resistance values are fixed, and thus, the influence of the 20 internal circuits upon external circuits can be reduced.

25 • Especially, when V_{tol} varies by a two-bit width with respect to V_{ol} , impedance trimming can be carried out by using a code value (resistance value) at which V_{tol} is equal to V_{rl} . Accordingly, trimming of high accuracy can be executed.

FIGS. 30 and 31 show the essential elements of the

present invention which are used to accomplish these effects. The concept of the present invention is that for the resistance values of the resistance elements, the value R_{trim} is set so as to establish a 5 relationship closest to $R_{ext}:R_1 = R_{trim}:R_t$.

Further, it should be appreciated that within the scope of this concept, the following variations are possible.

• The P channel MOS transistor (current driver) is 10 connected to the power terminal VDD in order to increase an output current from a power amplifier.

• Likewise, a source follower of the N channel MOS transistor is connected to the power terminal VDD.

• The resistor R_1 is formed inside the LSI so that 15 the resistance value of the resistor R_1 can be varied in accordance with the resistance value of the external resistor R_{ext} .

• The code control circuit is composed of a latch and a coder instead of the multistage shift register.

• The number of states of a code signal is 20 increased or reduced on the basis of the relationship between the adjustable variation range and adjustment accuracy.

• Unit resistors of the same shape are arranged 25 close to each other within the LSI in order to improve the relative accuracy for the resistors R_1 and R_t .

• The relationship between the reference voltage

Vref and the power voltage VDD is kept constant, and the relationship between the power voltage VDD and ground voltage VGNBD of the whole circuit is reversed.

• The value for the resistor Rt is adjusted rather than adjusting the value for the resistor R1 in accordance with the value for the external resistor Rext and the parasitic resistance.

• A fixed ratio is maintained between the resistor Rtrim for a feedback system and an actual target impedance trimming resistor (an output driver section and an input resistance section).

• In the case where the code control circuit outputs codes the values of which decrease by degrees, the down detection signal generating circuit in the code flattening circuit is replaced by the up signal generating circuit.

The impedance trimming circuit according to the ninth embodiment of the present invention can be applied to various kinds of semiconductor integrated circuits which are required to execute impedance matching with respect to the output impedance, input impedance, terminal resistor, or the like.

As described above, according to the impedance trimming circuit according to the example of the present invention, an accurate trimming operation can be performed by eliminating the adverse effects of variations associated with the LSI manufacturing

process. Further, the circuit can be constructed using a reduced number of external parts, thus reducing manufacturing costs.

Additional advantages and modifications will 5 readily occur to those skilled in the art. Therefore, the invention in its broader aspects is not limited to the specific details and representative embodiments shown and described herein. Accordingly, various modifications may be made without departing from the 10 spirit or scope of the general inventive concept as defined by the appended claims and their equivalents.